



Blast Mitigation Effort

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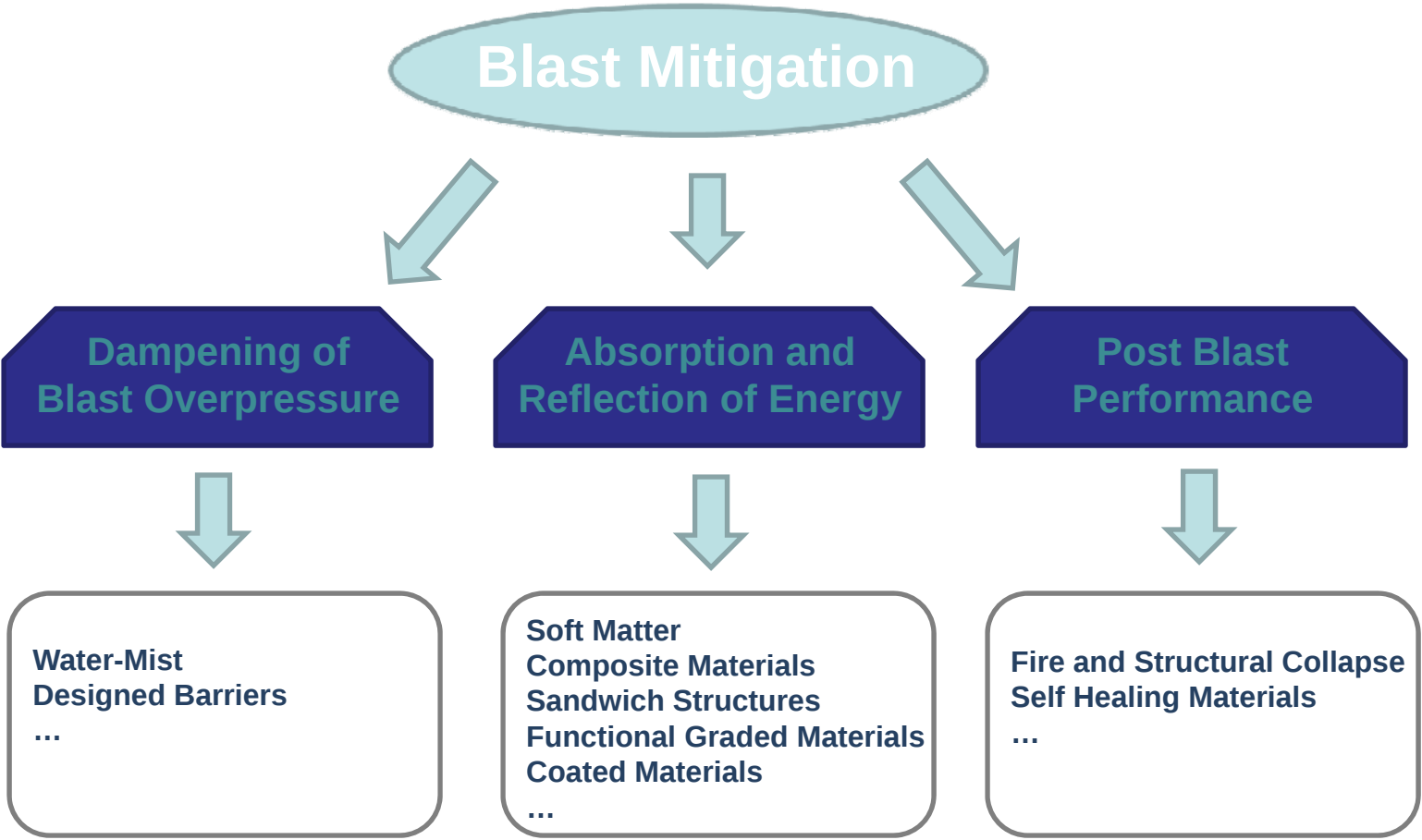
Northeastern University

Missouri Science & Technology

Washington State University



Introduction





Response of Sandwich Composite Panels to Shock Loading

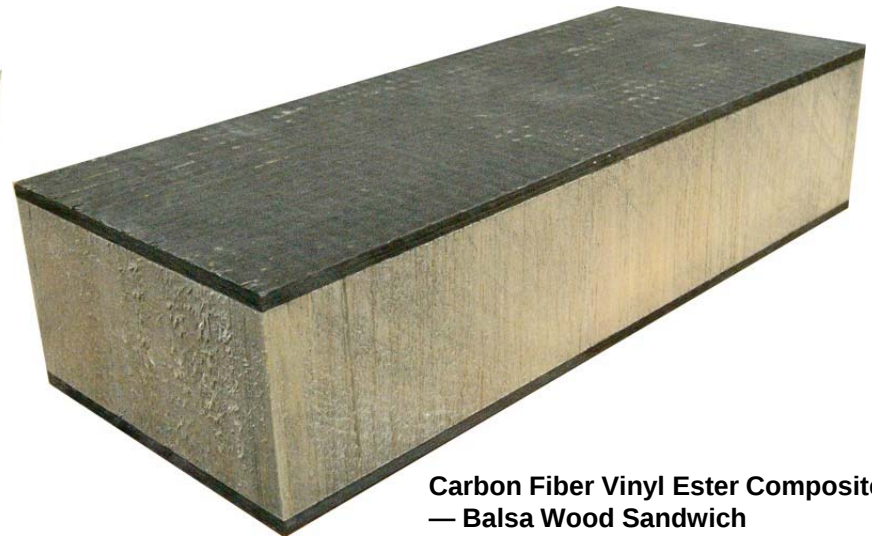


Sandwich Composites

These are materials consisting of two face sheets sandwiching a core material.



E-Glass Vinyl Ester Composite
— Corecell Foam Sandwich



Carbon Fiber Vinyl Ester Composite
— Balsa Wood Sandwich

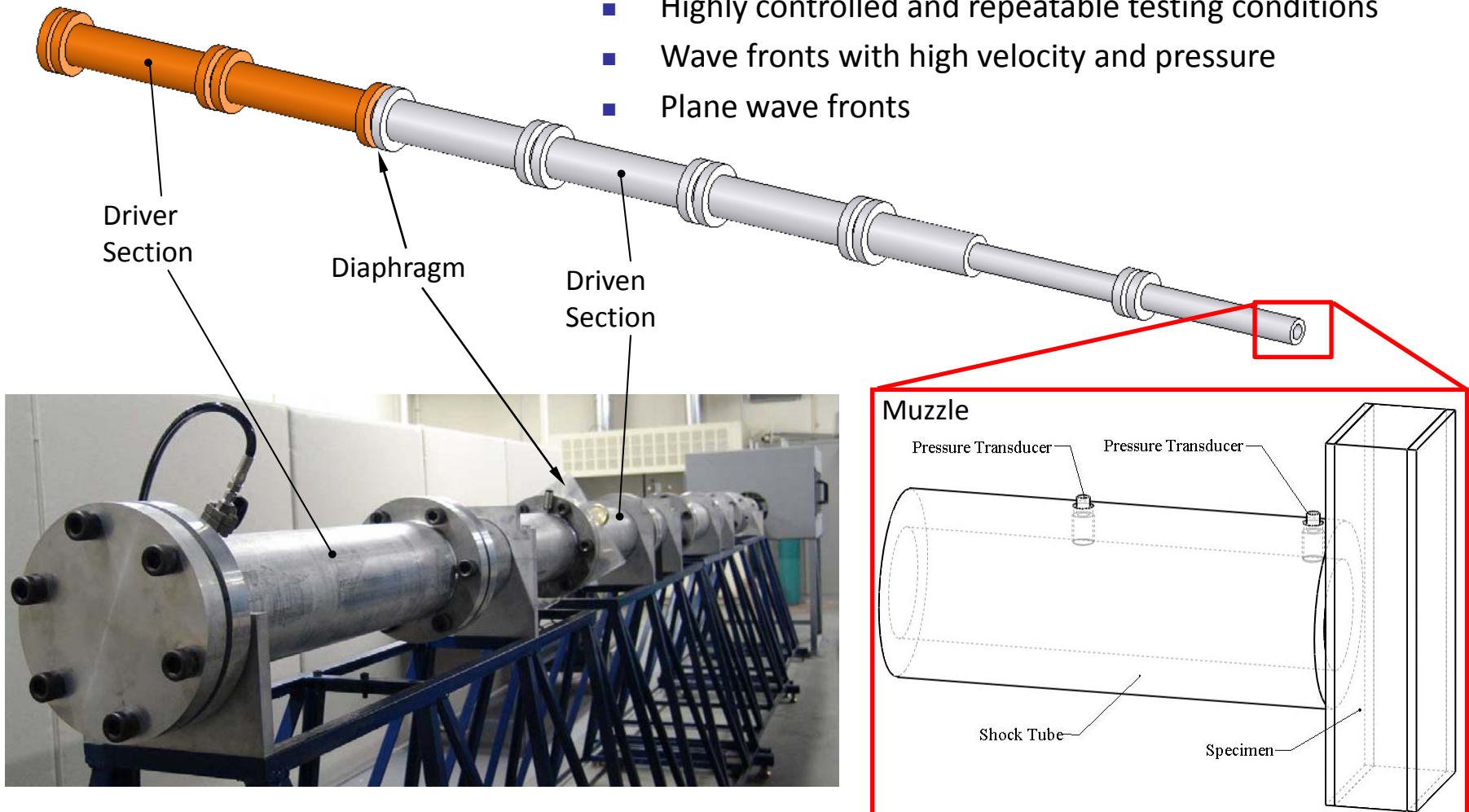
Advantages:

- ☐ *High strength and stiffness per unit weight*
- ☐ *Good thermal insulation*
- ☐ *High energy absorption*

Shock Tube

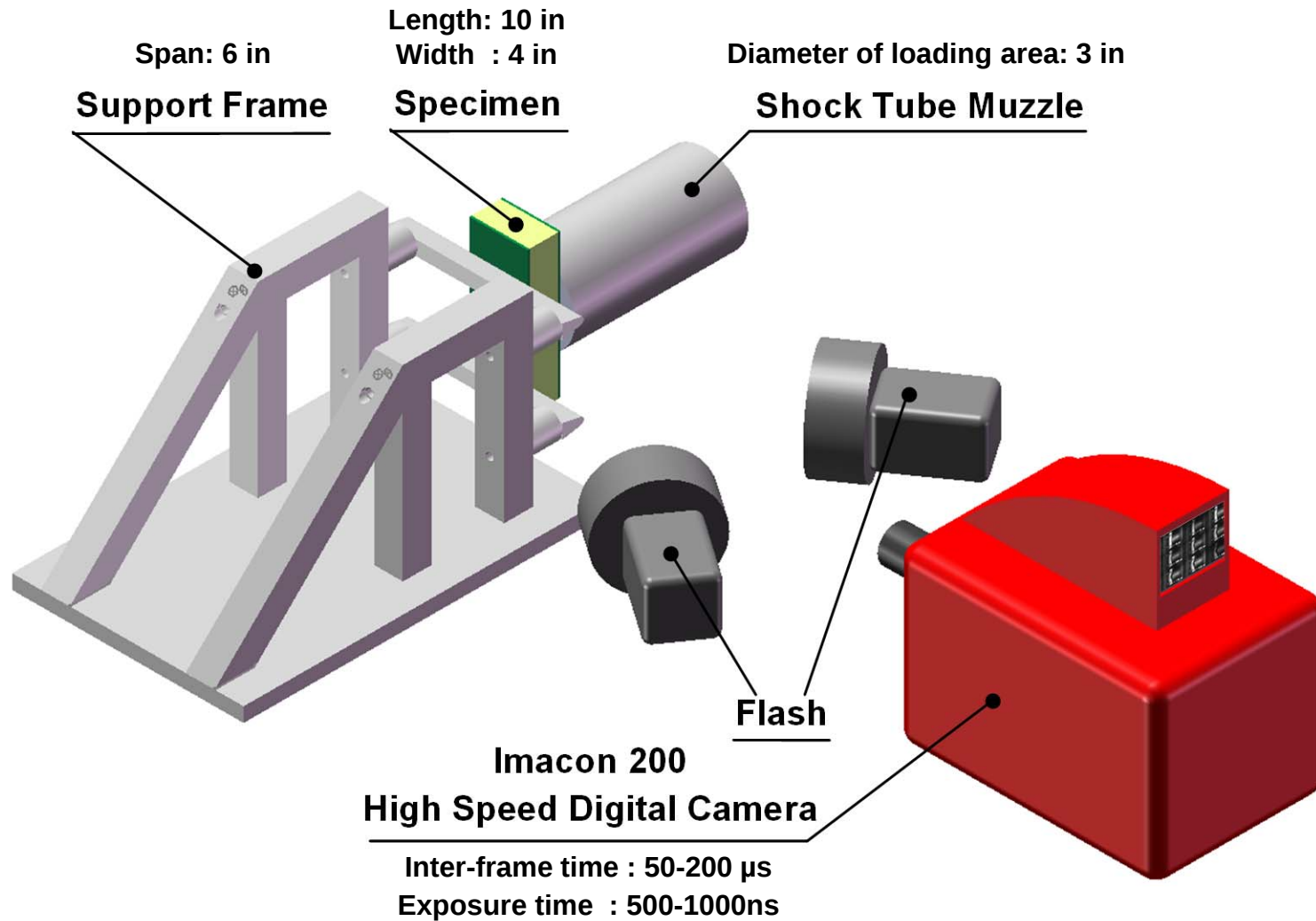
Advantages

- Highly controlled and repeatable testing conditions
- Wave fronts with high velocity and pressure
- Plane wave fronts





Experimental Setup





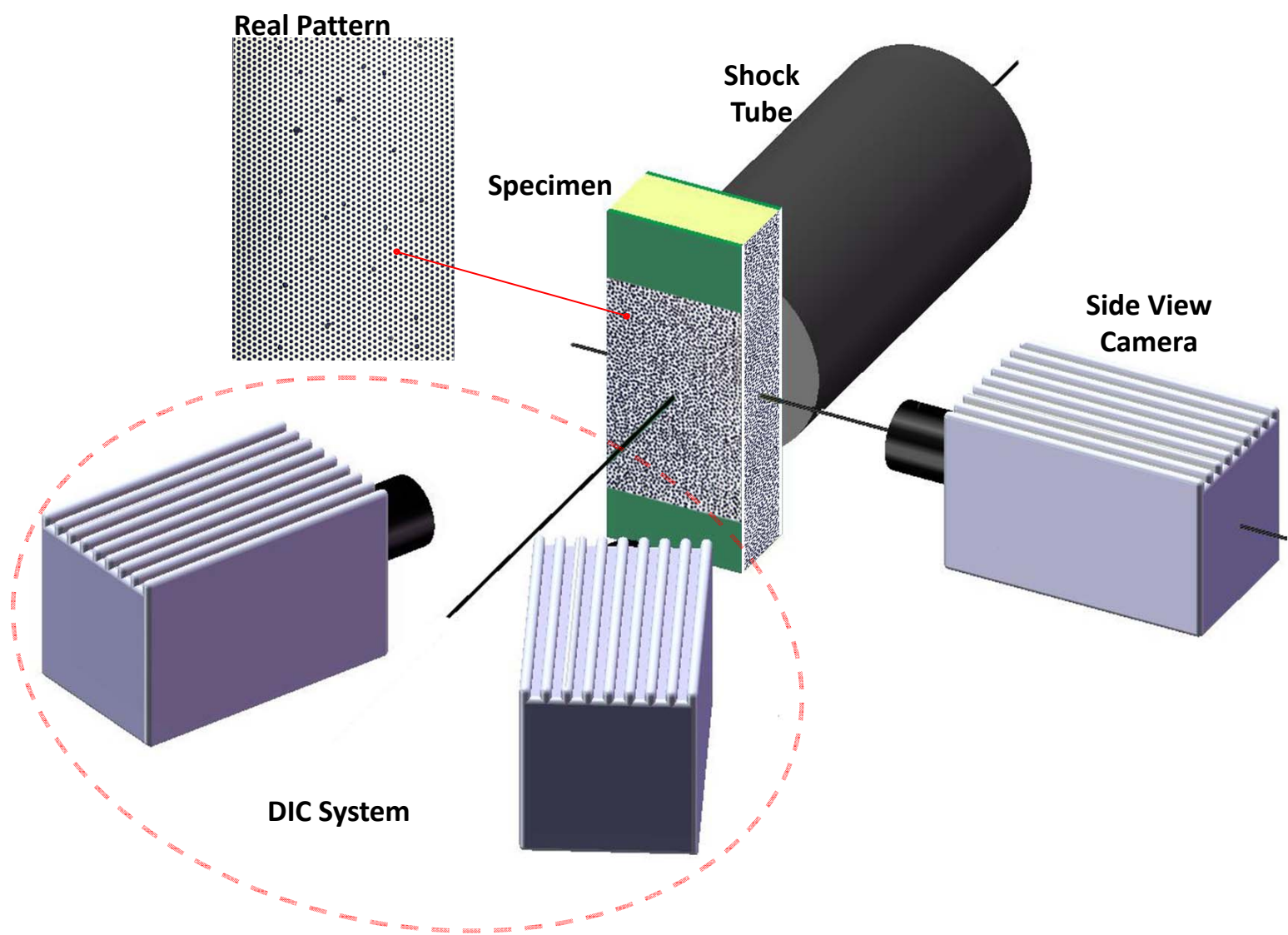
Real Time Observation



E-Glass Vinyl Ester Composite — Corecell Foam Sandwich under blast load

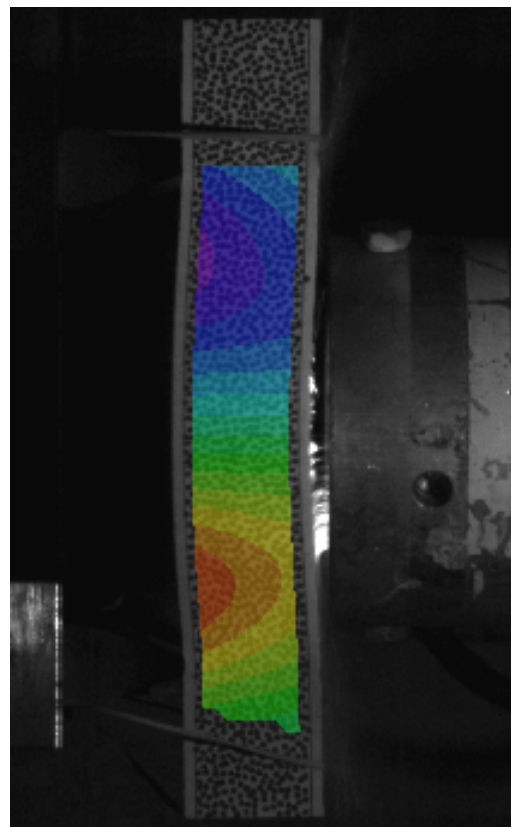


DIC Experimental Setup

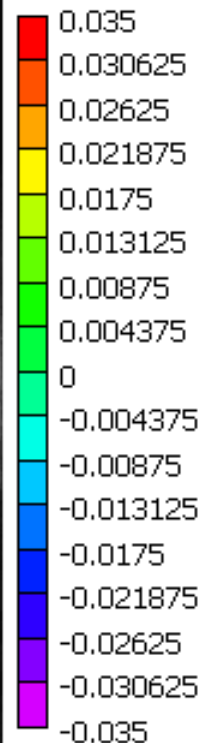




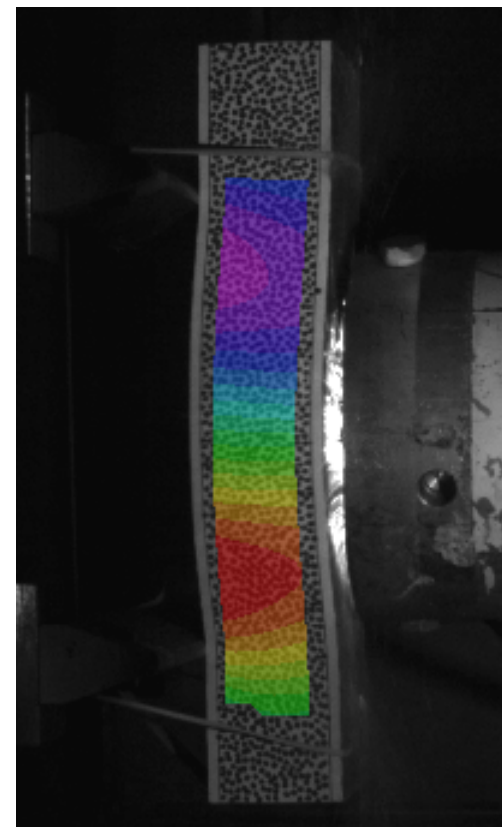
Shear Strains in the Core 2-D and 3-D DIC System



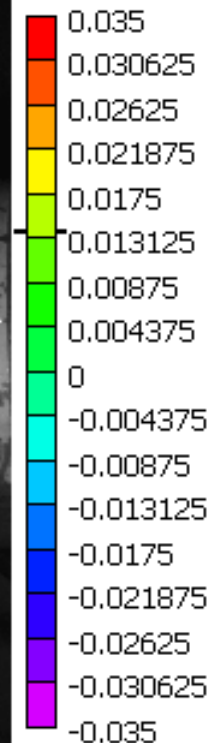
exy [1] - Lagrange



2-D DIC



exy [1] - Lagrange

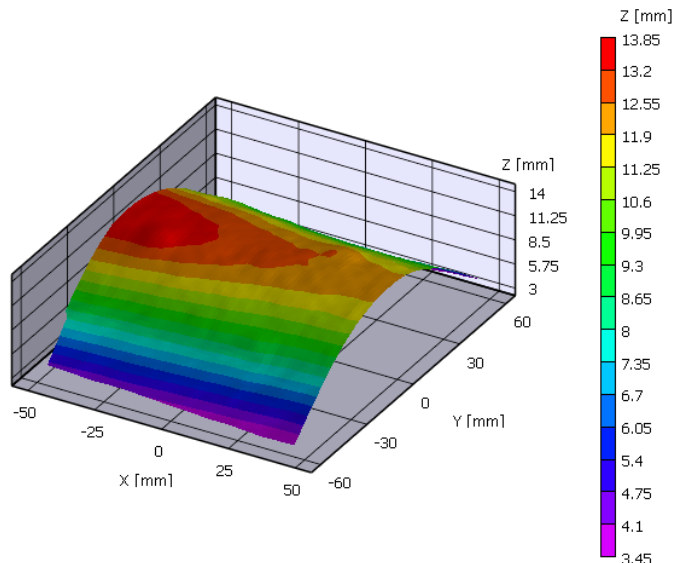
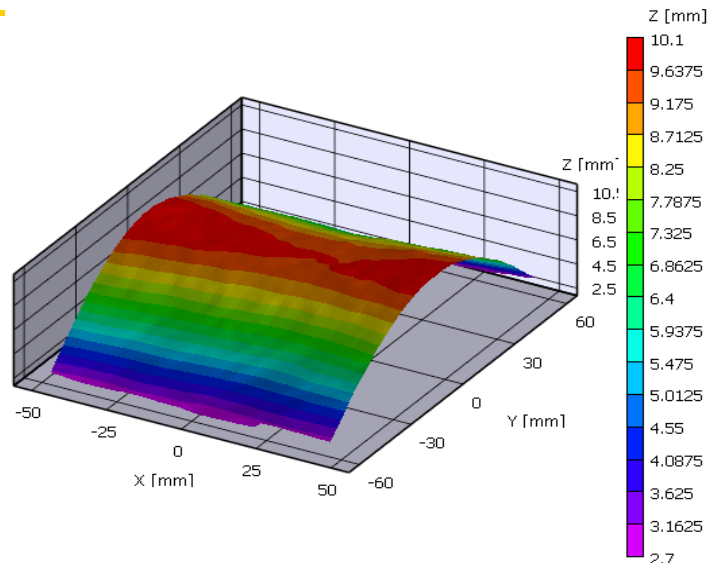


3-D DIC

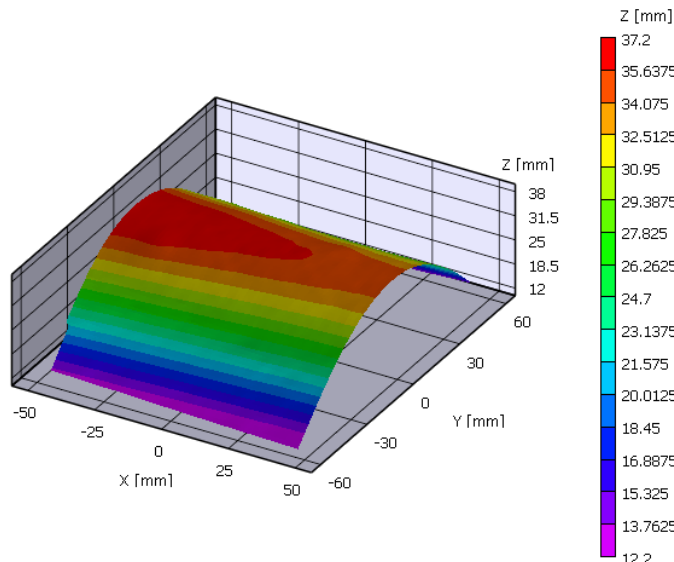
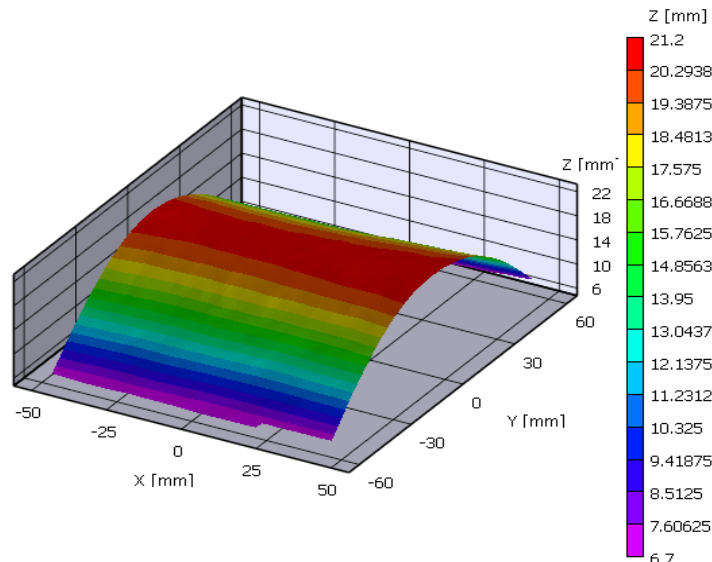


3D-Deflections

600 microseconds



1800 microseconds



PU Back

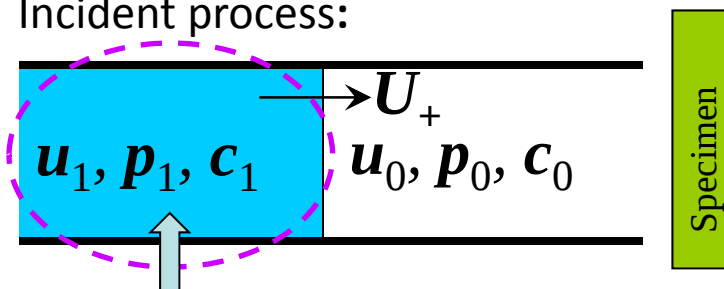
PU Front



Energy Calculation

Incident and Remaining Energy Calculations:

Incident process:



Incident Energy:

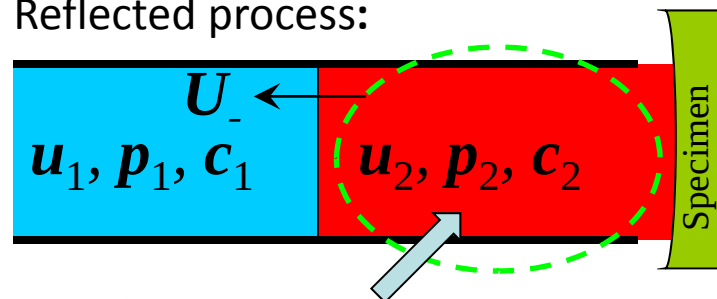
energy stored in the impinging gas

$$\frac{p_2}{p_1} = (1 + \mu^2) \left(\frac{u_1 + U_+}{c_1} \right)^2 - \mu^2$$

$$(1 - \mu^2)(U_+ - u_0)^2 - (u_1 - u_0)(U_+ - u_0) = (1 - \mu^2)c_0^2$$

$$(1 - \mu^2)(U_- + u_1)^2 - (u_1 - u_2)(U_- + u_1) = (1 - \mu^2)c_1^2$$

Reflected process:



Remaining Energy:

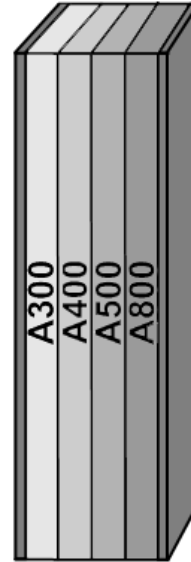
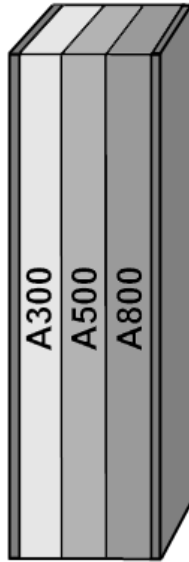
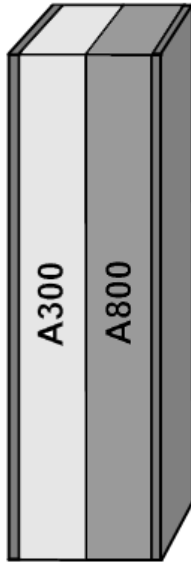
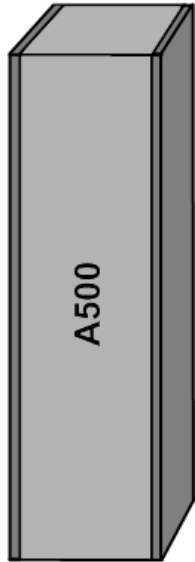
energy stored in the gas located
behind the reflected shock front

$$E = \int \left[(\text{pressure}) \times \left(\frac{\text{cross-section}}{\text{area}} \right) \times \left(\frac{\text{gas particle}}{\text{speed}} \right) \right] dt$$

Specimen Configurations

(Monotonically Increasing Wave Impedance)

Configurations



Specimen Dimensions:

- **Total length:**
254 mm (10 in)
- **Total width:**
101.6 mm (4 in)
- **Total thickness:**
48 mm (1.9 in)
- **Face sheet thickness:**
5 mm (0.2 in)

Specimens

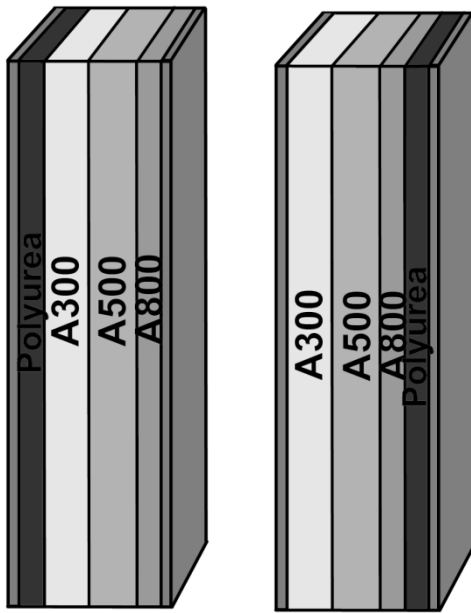


Gradation	Average Areal Density (kg/m ²)
1 Layer	19.12
2 Layer	18.43
3 Layer	19.02
4 Layer	20.07



Specimens and Configurations

Configurations



Average Areal Density: 26 kg/m²

Specimens



PU Front

PU Back

Dragonshield HT Properties

DRY PROPERTIES @ 34 MILS (0.8 mm)		
Tensile Strength	ASTM D-638	4219 psi (29.3 mpa)
Elongation @ 77°F (25°C)	—	619%
Hardness (Shore D)	ASTM D-2240	52-44
100% Modulus	ASTM D-412	1280 psi (8.9 mps) ± 100
300% Modulus	ASTM D-412	2137 psi (14.9 mpa) ± 100



High Speed Video



PU Front (Sample 3)



PU Back (Sample 4)



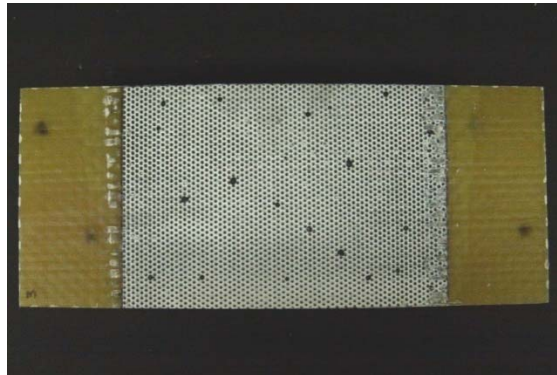
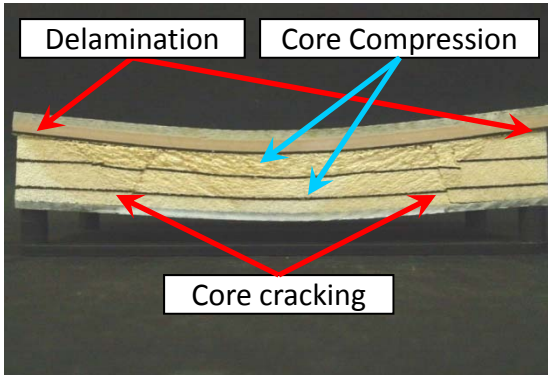
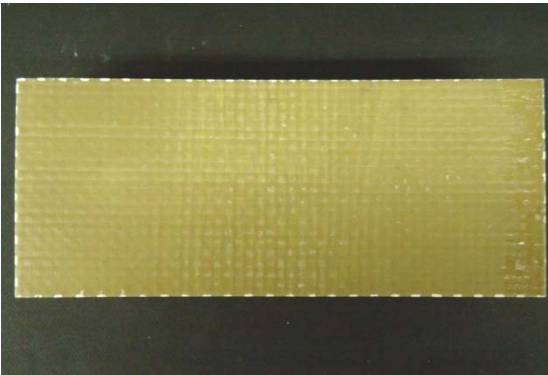
Post-Mortem Images

Front face sheet
(blast side)

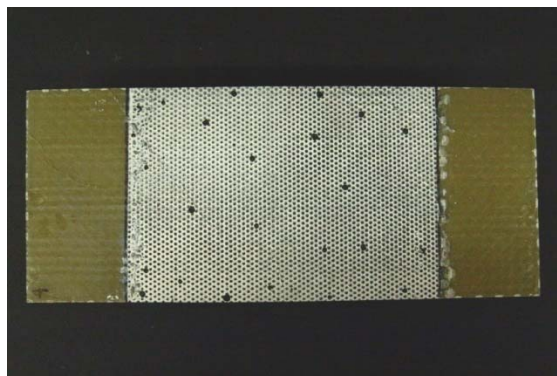
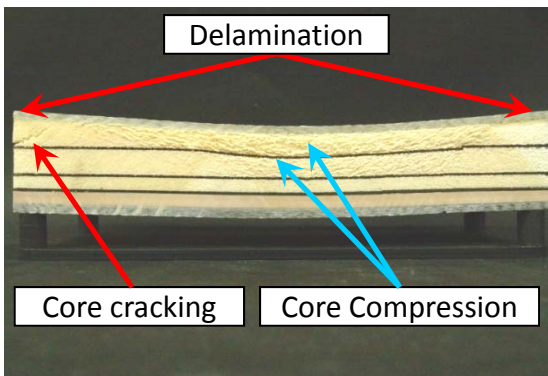
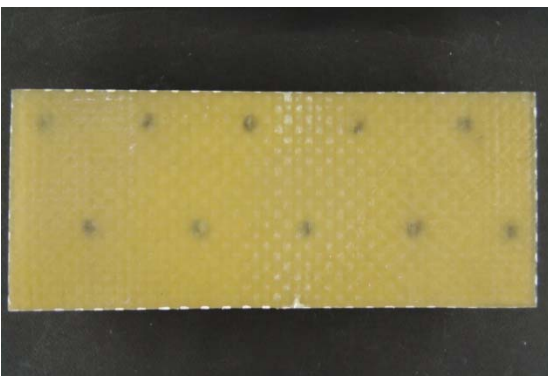
Foam core

Back face sheet

PU Front



PU Back

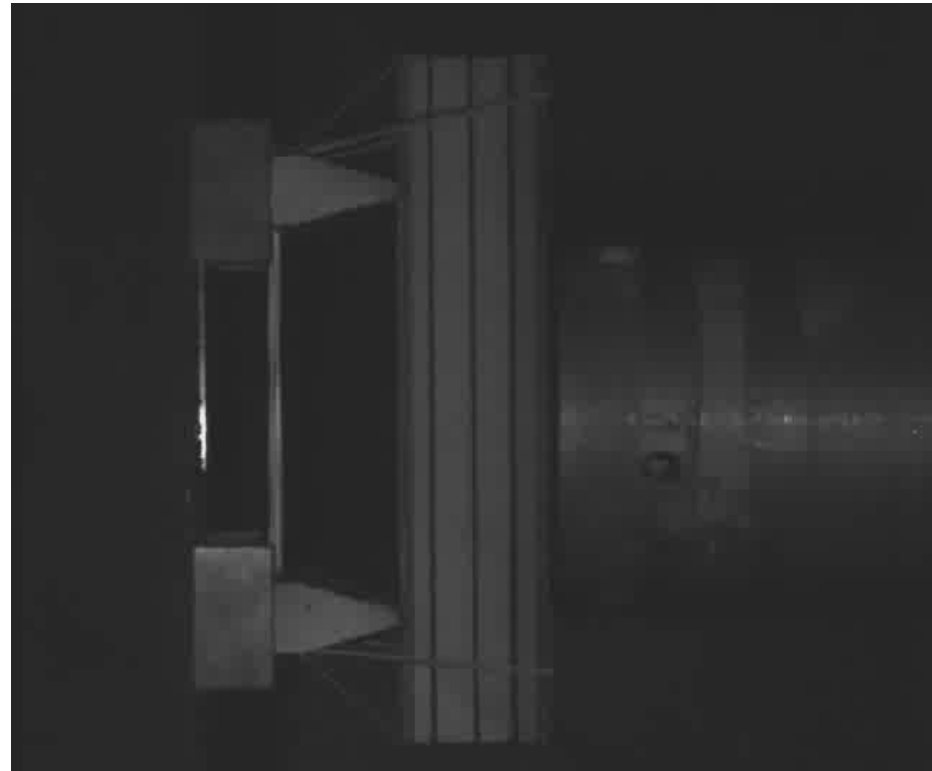




High Speed Video (10 plys)



PU Back(Sample 1)



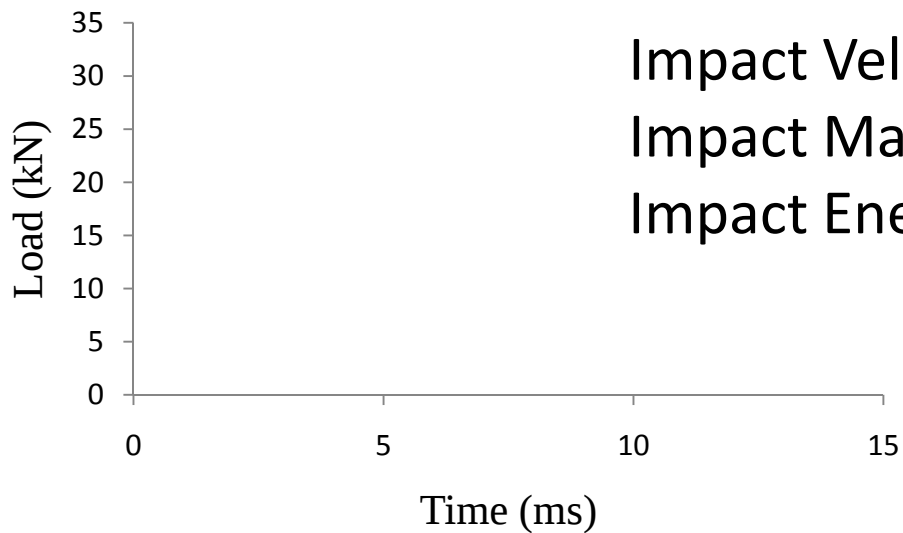
PU Front (Sample 3)



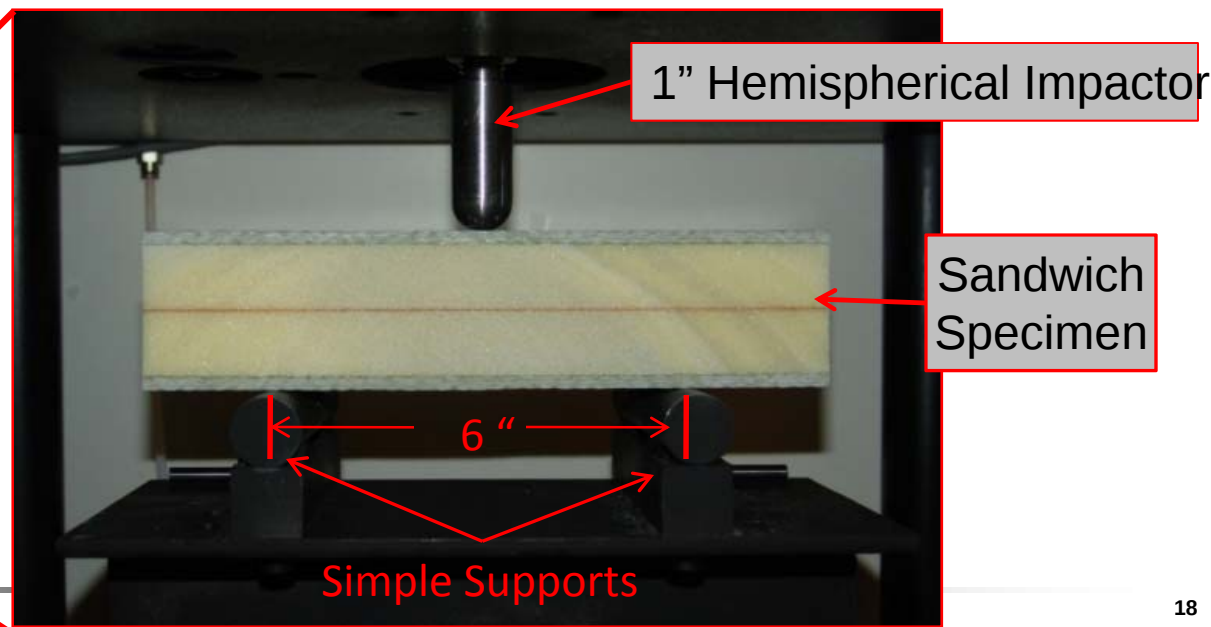
The Effect of Low and High Velocity Impact Damage on Blast Performance



Low Velocity Impact Experiment

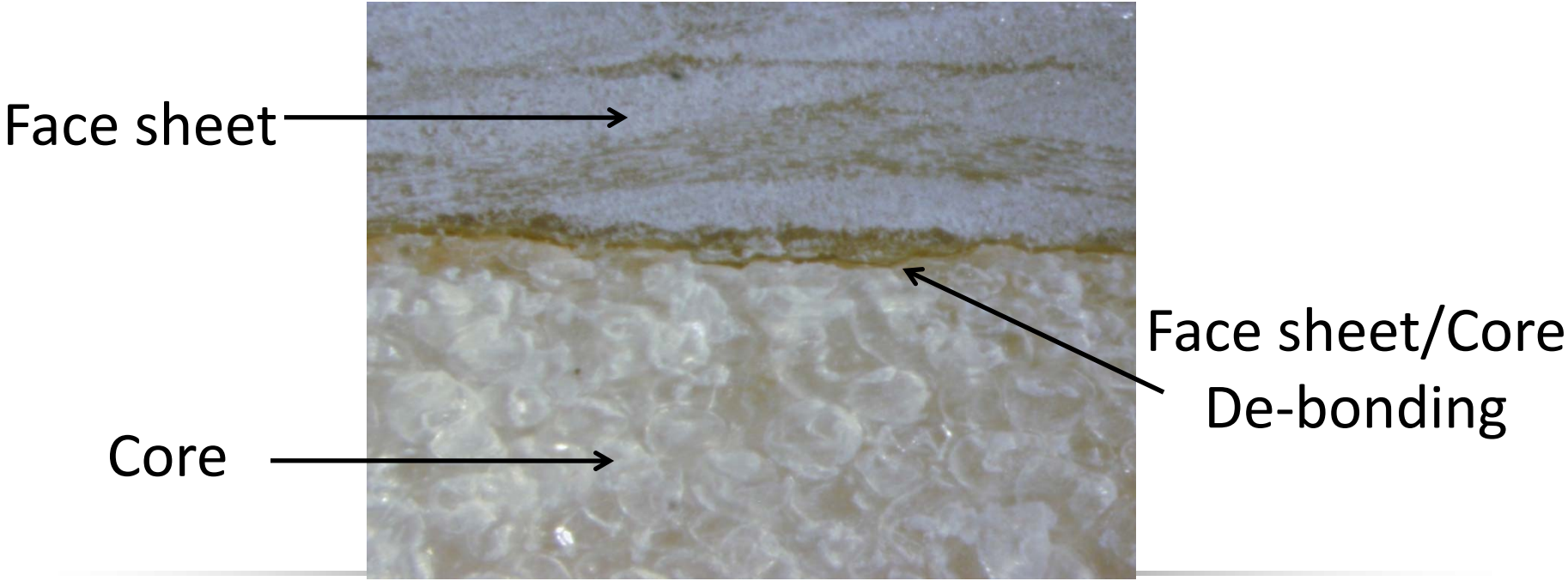
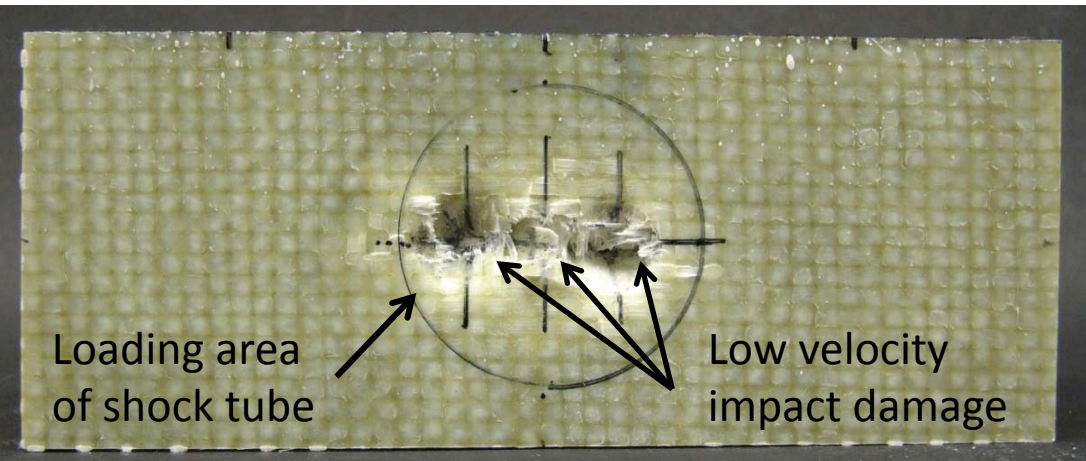


Impact Velocity ≈ 4.7 m/s
Impact Mass ≈ 26.1 kg
Impact Energy ≈ 300 J

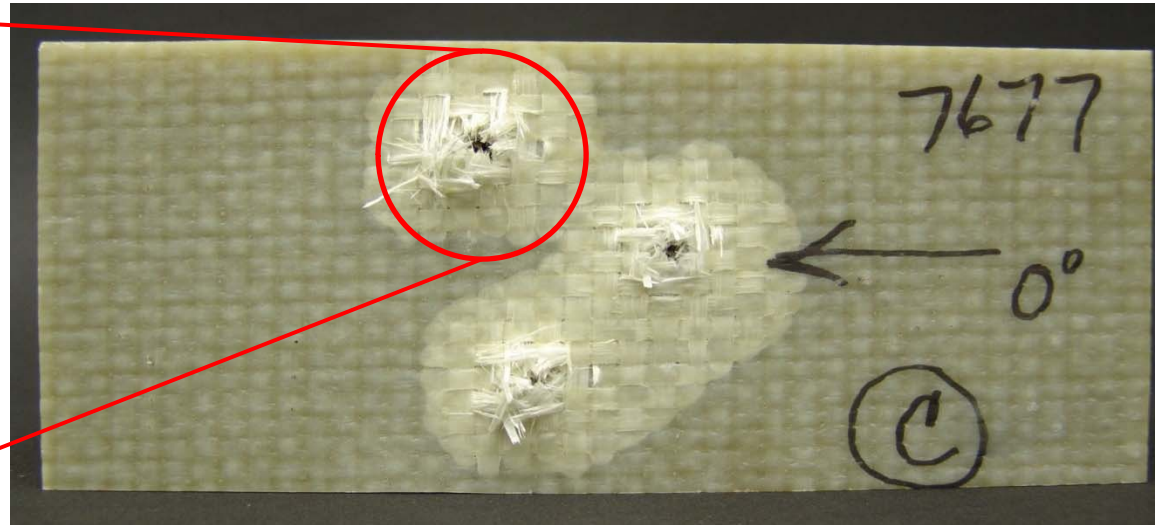
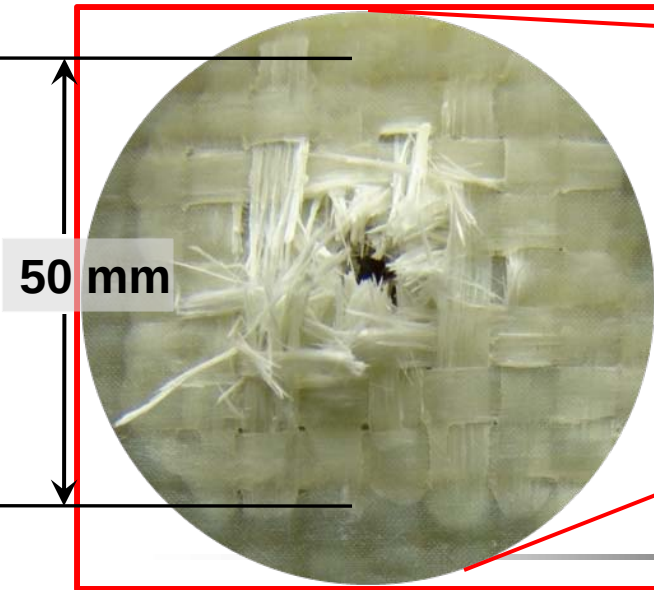
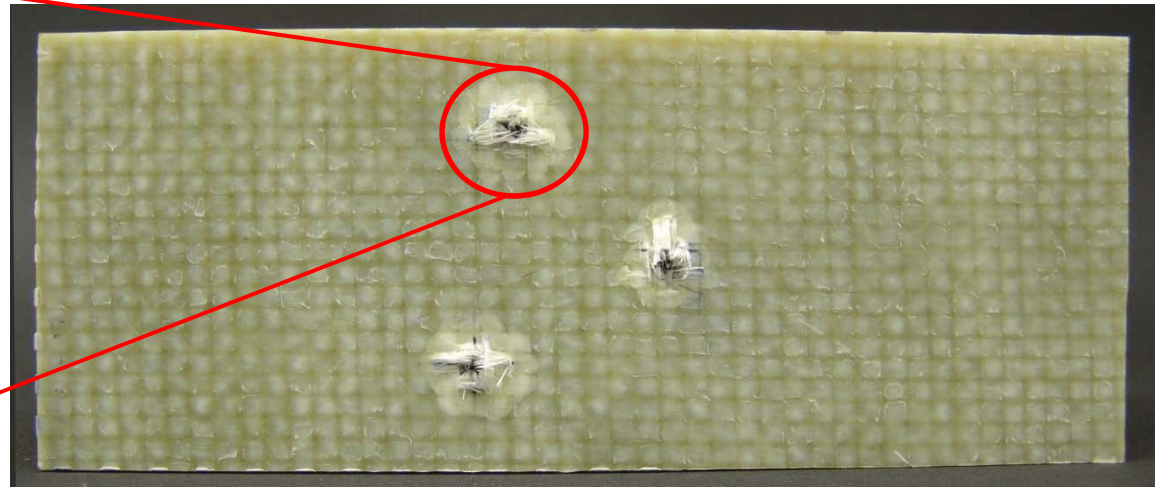
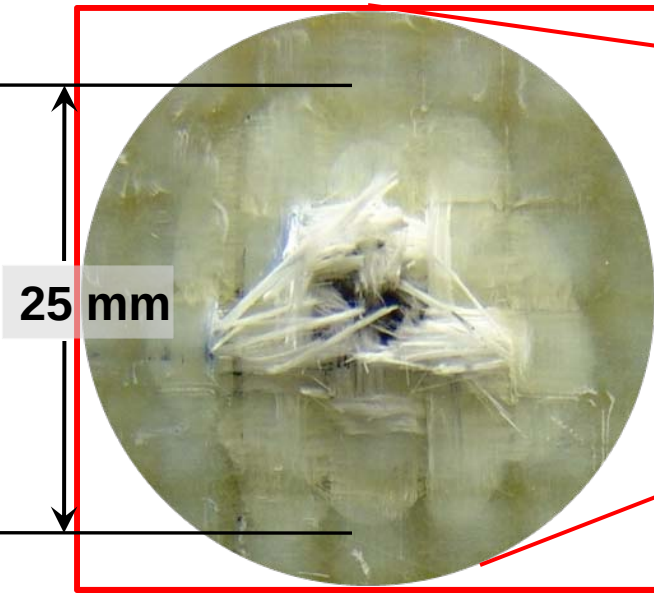




Typical Low Velocity Impact Damage

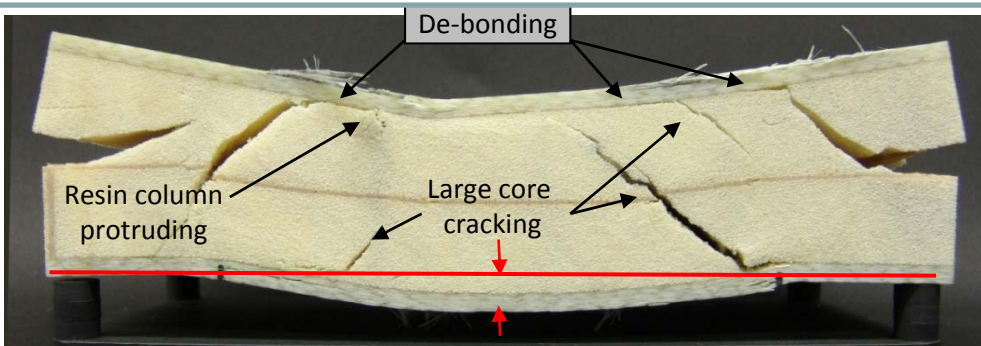


Typical High Velocity Impact Damage





Post Blast Images of Pre Damaged Sandwich Composites



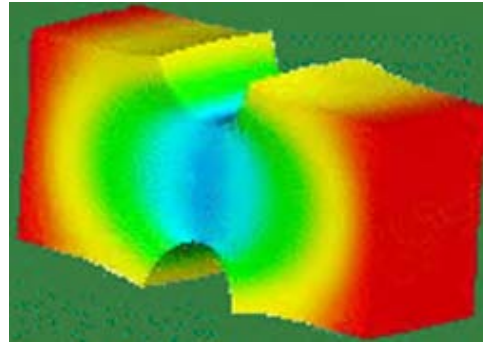
Specimen with High Velocity Impact Damage

Impact Type: High Velocity (920 m/s)
Number of Impacts: 5
Impact Mass : 0.01Kg
Total impact Energy Absorbed: $\approx 2108J$



Specimen with Low Velocity Impact Damage

Impact Type: Low Velocity (4.7 m/s)
Number of Impacts: 3
Impact Mass : 26.21 kg
Total impact Energy Absorbed: $\approx 760J$



IMPLAST 2010

Renaissance Providence Hotel

12-14 October 2010

Workshop on Blast Mitigation

Keynote Speakers

Dr. Gerald Nurick, University of Capetown, South Africa

Dr. Mary Ellen Hynes, Department of Homeland Security, USA

Dr. Ravinder Chona, Air Force Research Laboratories, USA

Dr. William G. Proud, Cavendish Laboratories, Cambridge, UK

Dr. Yapa D.S. Rajapakse, Office of Naval Research, USA